





# **CFD-based Approach For Prediction Of Headspace Pressure In Can During Thermal Sterilization Of Foods**



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#### Introduction

Numerical Modelling

Results

Conclusion and perspectives



## What is Thermal Sterilization?







Raw Food



Thermal sterilization using Retort

- Heat treatment above 100°C
- Destroys heat-resistant spores



Canned Foods with longer shelf life (eg.  $\geq$  2 years)





СТСРА

#### Introduction

Results

Context

### **Retort Overview**



Schematic of a conventional retort for thermal sterilization



#### Introduction

Numerical Modelling

Results

#### **Challenge and Goal**

## **Headspace Pressure**



### Challenge

- Measuring headspace pressure due to water vapour in the food industry is a big challenge.
- External counter-pressure is required to tackle inner pressure generated in canned foods which is related to headspace pressure.

#### Goal

 To predict local temperatures and internal headspace pressure in cans during thermal sterilization process, which accounts for water vapor generation and dry air pressure in the headspace.

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Numerical Modelling

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Conclusion and perspectives

### Materials and Methods

### **Experimental Setup**



STERITECH Retort in Oniris, Nantes, France



Schematic of experimental setting

Numerical Modelling

Results

Conclusion and perspectives

### Materials and Methods

### **Experimental Setup**

RÉPUBLIQUE FRANÇAISE



3 cans for top temperature



3 cans for center temperature



3 cans for headspace temperature



3 cans for bottom temperature

Mass of mashed potato = 279.96 ± 0.42 g



**Temperature probes** 

Pressure sensor inside cans

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Governing Equations

# **Numerical Modelling: Governing Equations**

Heat Transfer in Solids (mashed potato)

$$\rho C_p \frac{\partial T}{\partial t} - \nabla (-k\nabla T) = 0$$
<sup>(1)</sup>

+Initial Conditions +Boundary Conditions  $T_{initial} = 20^{\circ}C$ 

$$-n.q = q_0 \tag{2}$$

$$q_0 = h_{global}(T_{retort} - T)$$
(3)

Heat Transfer in Fluids (air at the headspace)

$$\rho C_p \frac{\partial T}{\partial t} + \rho C_p \boldsymbol{u} \cdot \nabla T - \nabla \cdot (k \nabla T) = 0 \qquad (4)$$

+Initial Conditions + Boundary Conditions

RÉPUBLIQUE FRANCAISE CTCP/

Dairon

Fluid Mechanics : Navier-Stokes equations with the Boussinesq approximation (air at the headspace)

$$\rho \frac{\partial \boldsymbol{u}}{\partial t} = -\nabla p + \mu \nabla^2 \boldsymbol{u} + F \tag{5}$$

$$F = \rho g \tag{6}$$

+Initial Conditions +Boundary Conditions p = 1 [atm]

$$\boldsymbol{u}_{initial} = \boldsymbol{0} \tag{7}$$

#### Ideal gas law for dry air at the headspace

$$\mathsf{P}V = nRT \tag{8}$$





GEPEA





# **Conclusions and Perspectives**

The numerical model coupled to the experimental investigation enables to:

- Predict local temperature profiles at different locations in canned foods.
- Predict dry air pressure in the headspace.
- Estimate the water vapour pressure contributing towards headspace pressure
- Evaluate the mass of water vapour generated during the thermal sterilization process.

#### Perspectives

Improvement of the numerical model by integrating water vapour evaporation flux in the CFD model.





## **Thank You Very Much For Your Attention**

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